

neutron electric dipole search at TRIUMF

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for TUCAN collaboration



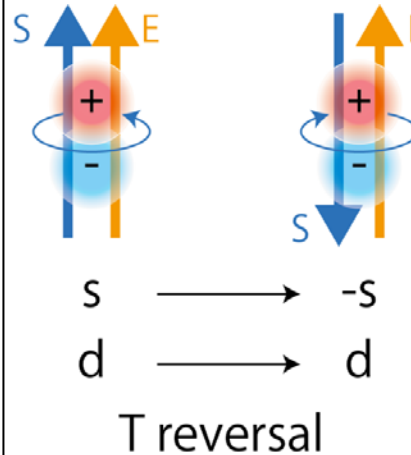
outline

- Neutron electric dipole moment
- Ultra-cold Neutron (UCN)
- UCN production by super thermal method
- UCN source at TRIUMF
 - Vertical source
 - developed at RCNP
 - first UCN production at TRIUMF on November 13, 2017
 - UCN source upgrade
 - LD2 moderator
 - High cooling power helium cryostat
 - expected statistics

Neutron Electric Dipole Moment (nEDM)

Sakharov conditions
Baryogenesis

1. Baryon number violation.
2. C-symmetry and CP-symmetry violation.
3. Interactions out of thermal equilibrium.



• Electric Dipole moment

– Vector derived from charge distribution

$$\vec{d} = d \frac{\vec{s}}{|\vec{s}|} \quad \text{unit: e cm}$$

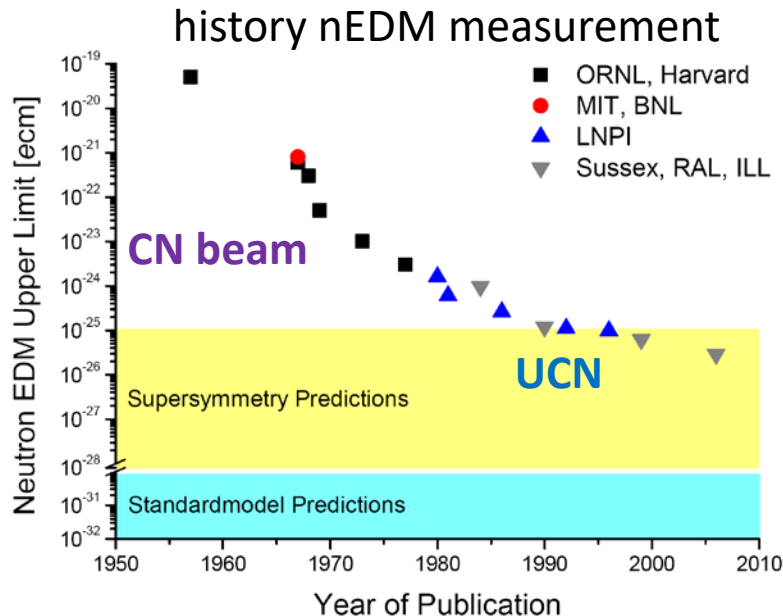
$d \neq 0 \rightarrow$ T violation

Assume CPT conservation

\rightarrow CP Violation

nEDM prediction

$$\text{SM} \sim 10^{-32} \text{ ecm}$$



Probe of beyond SM physics

current upper limit of nEDM

$$3.0 \times 10^{-26} \text{ ecm} \quad \text{@ILL, Grenoble}$$

$$\text{statistics} \quad 1.5 \times 10^{-26} \text{ ecm}$$

$$\text{systematics} \quad 0.7 \times 10^{-26} \text{ ecm}$$

Statistically limited

\rightarrow necessity of high intensity UCN source

How to measure nEDM?

Measure precession frequency under electro-magnetic field

$$H = -\vec{\mu} \cdot \vec{B} + \vec{d} \cdot \vec{E}$$

precession frequency

$$\hbar\omega = 2\mu_n B \pm 2d_n E$$

difference

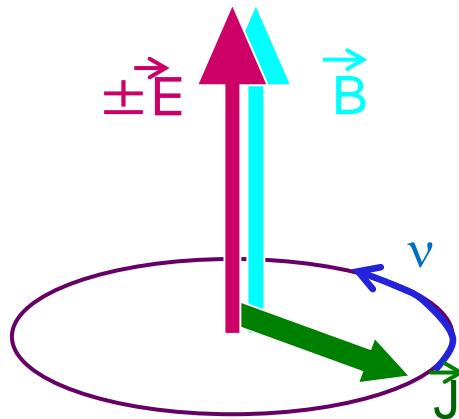
$$\Delta\omega = \omega_{\uparrow\uparrow} - \omega_{\uparrow\downarrow} = \frac{4dE}{\hbar}$$

in case of $E = 10\text{kV/cm}$, $d = 10^{-27}\text{ecm}$

$$\Delta\omega = 4 \times 10^{-7}\text{Hz}$$

cf. Larmor frequency of neutron

$$30\text{Hz} @ B_0 = 1\mu\text{T}$$



$$\hbar\omega = 2\mu_n B \pm 2d_n E$$

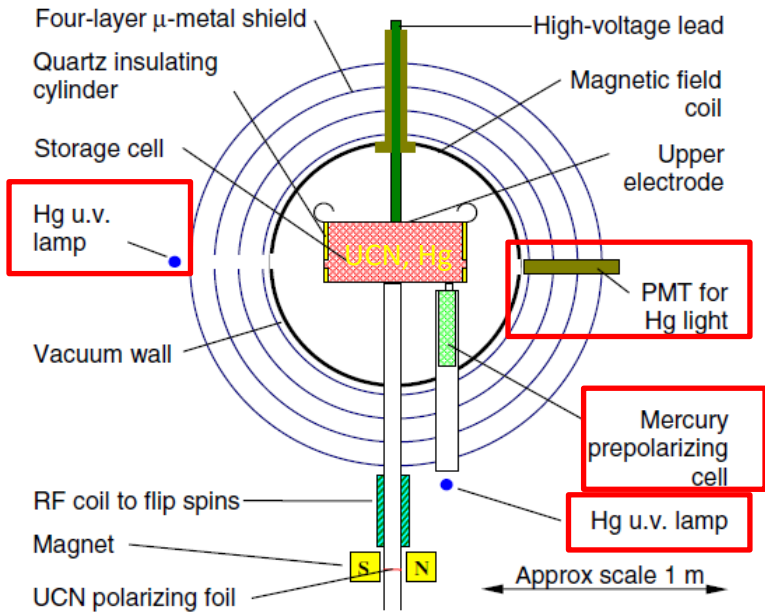
accuracy of 10^8

→ High frequency determination accuracy
(Ramsey resonance technique)

and

→ High field stability
→ Co-magnetometer

co-magnetometer



frequency shift

$$\Delta\omega = 4 \times 10^{-7} \text{ Hz}$$

($E = 10 \text{ kV/cm}$, $d = 10^{-27} \text{ ecm}$)

cf. Larmor frequency of neutron

$$30 \text{ Hz @ } B_0 = 1 \mu\text{T}$$

required magnetic field stability : 10^8 !!

$$1 \mu\text{T} * 10^{-8} = 10 \text{ fT}$$

It is difficult to stabilize magnetic field to such an accuracy

-> monitor and correct magnetic field

co-magnetometer

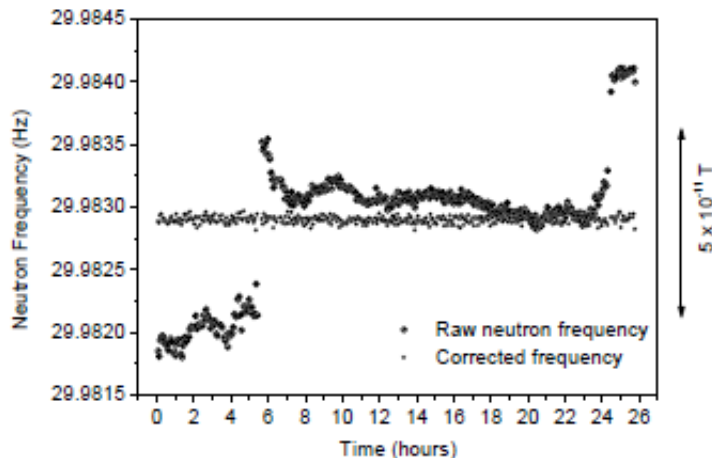
- feels same magnetic field as UCN

ILL use ^{199}Hg co-magnetometer

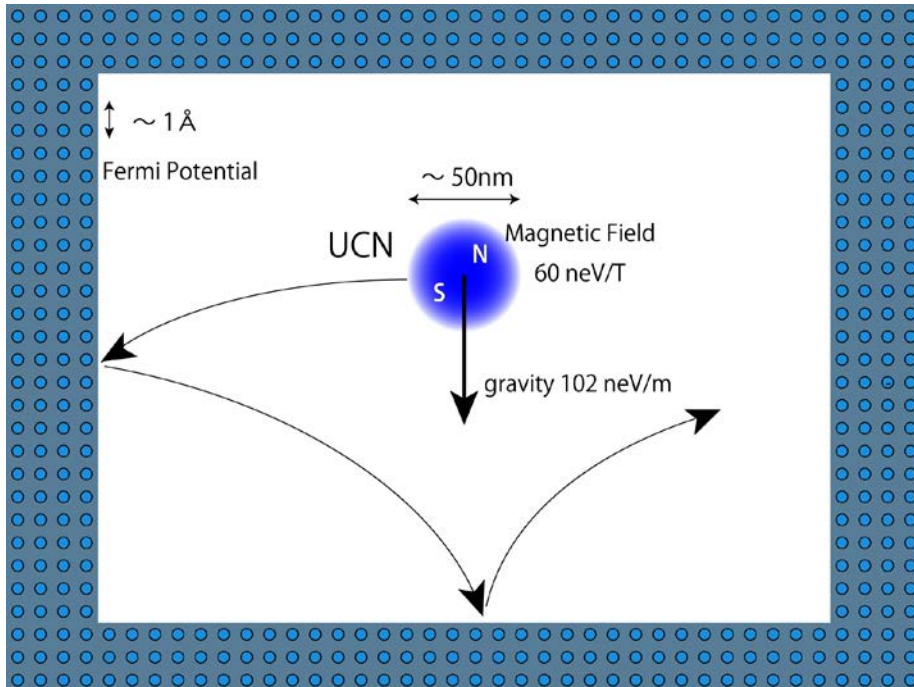
- polarization is measured by UV laser

Our plan : ^{199}Hg , ^{129}Xe dual co-magnetometer

- monitor magnetic field strength and gradient



Ultra Cold Neutron



Ultra Cold Neutron

Energy ~ 100 neV

Velocity ~ 5 m/s

Wave length ~ 50 nm

Interaction

Gravity 100 neV/m

Magnetic field 60 neV/T

Weak interaction

β -decay $n \rightarrow p + e$

Strong interaction

Fermi potential 335 neV (^{58}Ni)

atom distance : $\sim \text{\AA}$

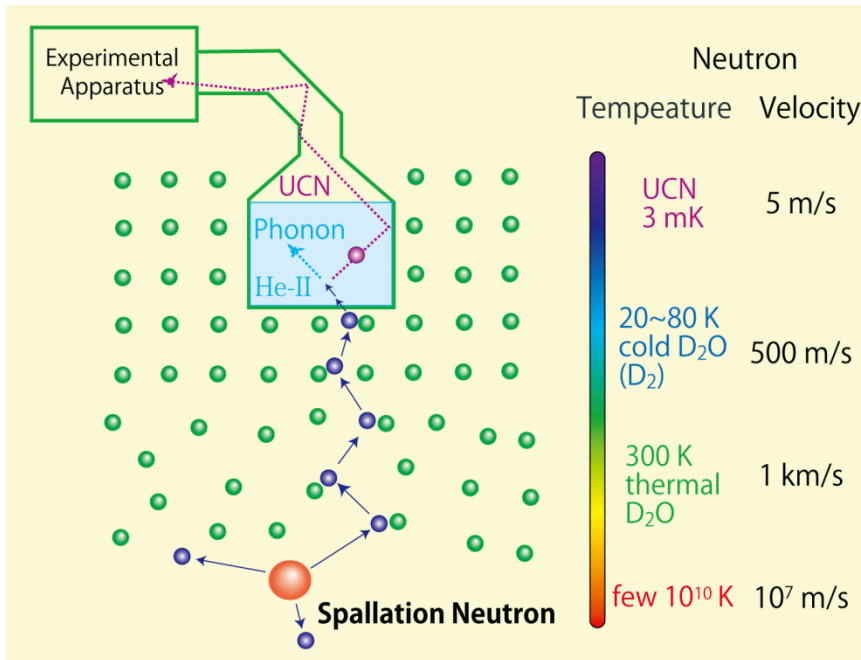
UCN feels average nuclear potential

UCN can be confined material bottle

→ Use in various experiments

nEDM, neutron lifetime, gravity, ...

UCN production by super fluid Helium



UCN production

spallation neutron

↓ D₂O, LD2 Moderator (300K, 20K)

cold neutron ~ meV

↓ Phonon scattering in He-II

Ultra cold neutron ~ 100neV

Feature of our source

▪ spallation neutron

High neutron flux

small distance between target and UCN production volume

▪ Super-fluid Helium (He-II) converter

long storage lifetime

important to accumulate UCN

Helium 4

- no neutron absorption cross section

- up-scattering by phonon

$$\tau_s = 600 \text{ s at } T_{\text{HeII}} = 0.8 \text{ K}$$

$$\tau_s = 36 \text{ s at } T_{\text{HeII}} = 1.2 \text{ K}$$

$$1/\tau_s \propto T^7$$

Vertical UCN source

- Vertical UCN source

- developed at RCNP

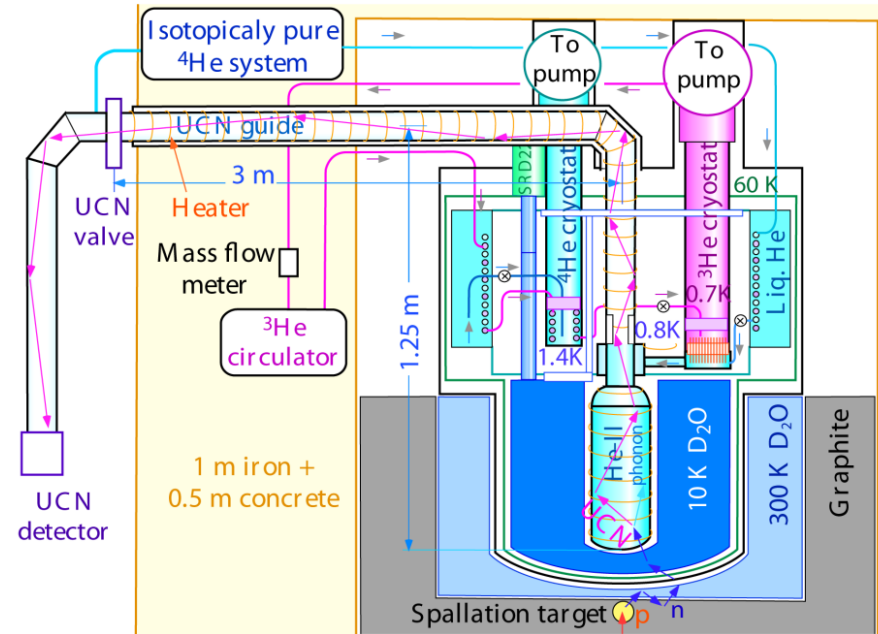
- $T_{\text{He-II}} : 0.8 \text{ K}$

- UCN life time: 81 sec

- UCN density: 9 UCN/cm^3

- $400 \text{ MeV} \times 1 \mu\text{A} = 0.4 \text{ kW}$

Y, Masuda et. al., Phys. Rev. Lett. 108, (2012), 134801



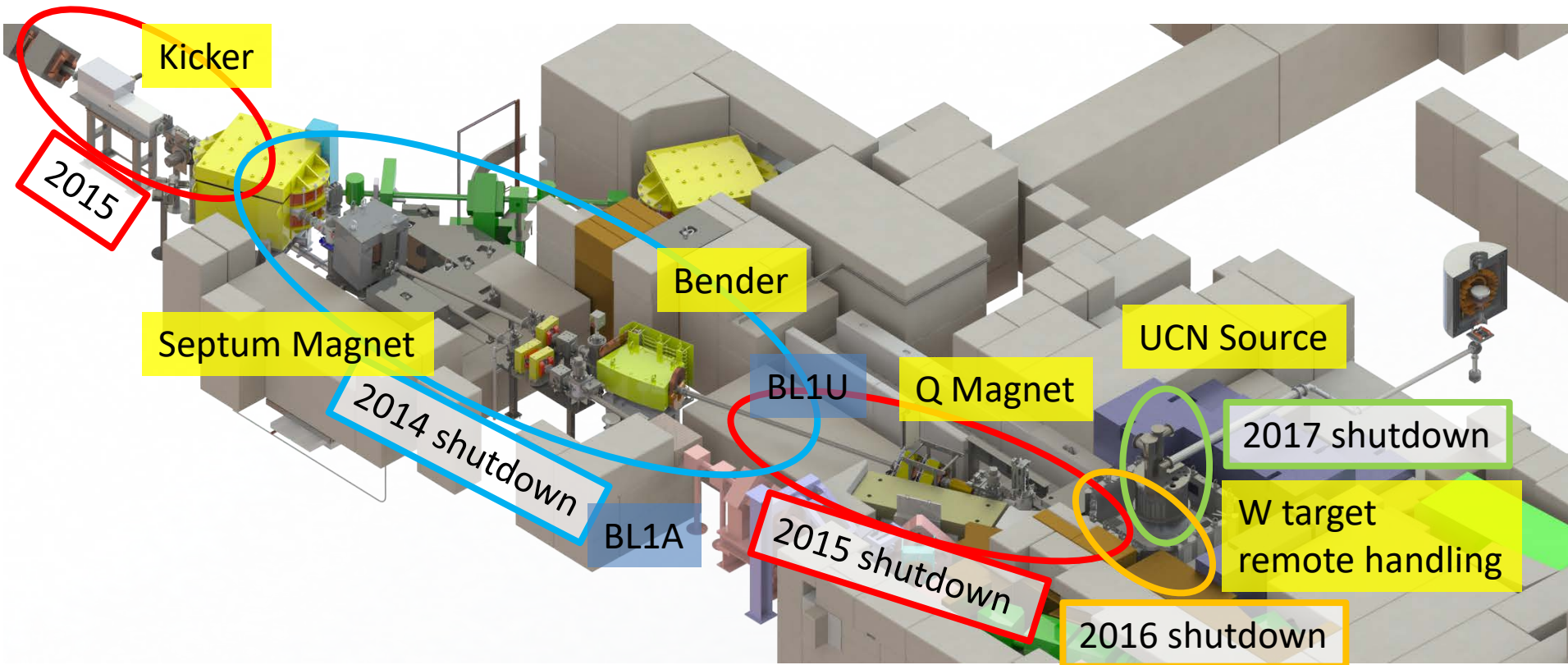
- move to TRIUMF

- modification for safety requirement

- 2017 Jan. – Apr. install at Meson hall

- 2017 Nov. UCN production SUCCEEDED!!

UCN Source @ TRIUMF

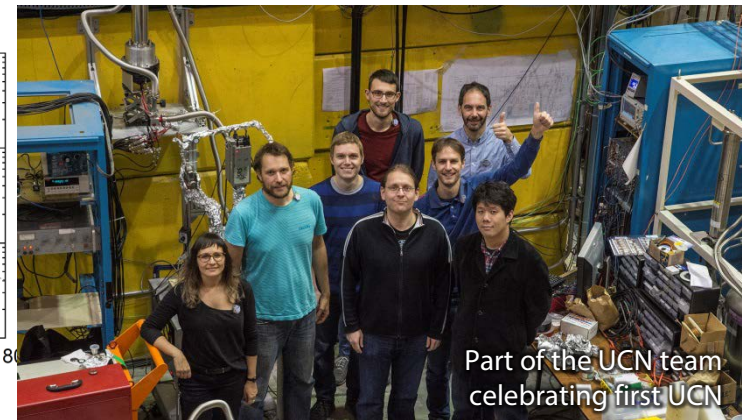
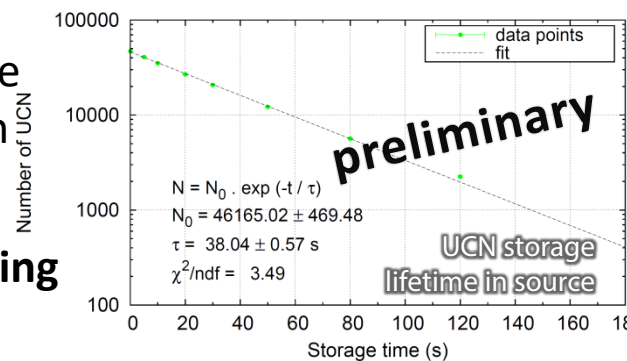
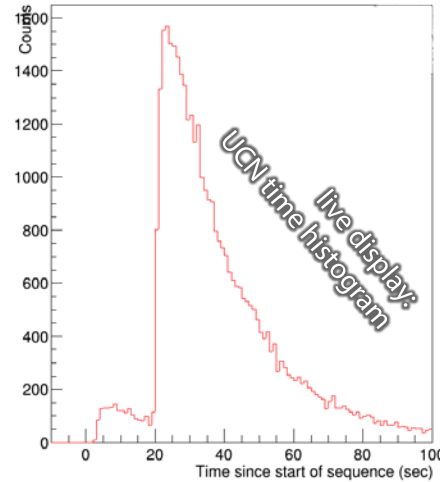


Major Milestone

- ✓ - 2016 proton beam line for UCN source (BL1U 500MeV, 40 μ A)
- ✓ 2016 commissioning proton beam line and cold neutron production
- ✓ 2017 UCN production by Vertical source (\sim 1 μ A)
- 2020 High intensity UCN source (40 μ A)

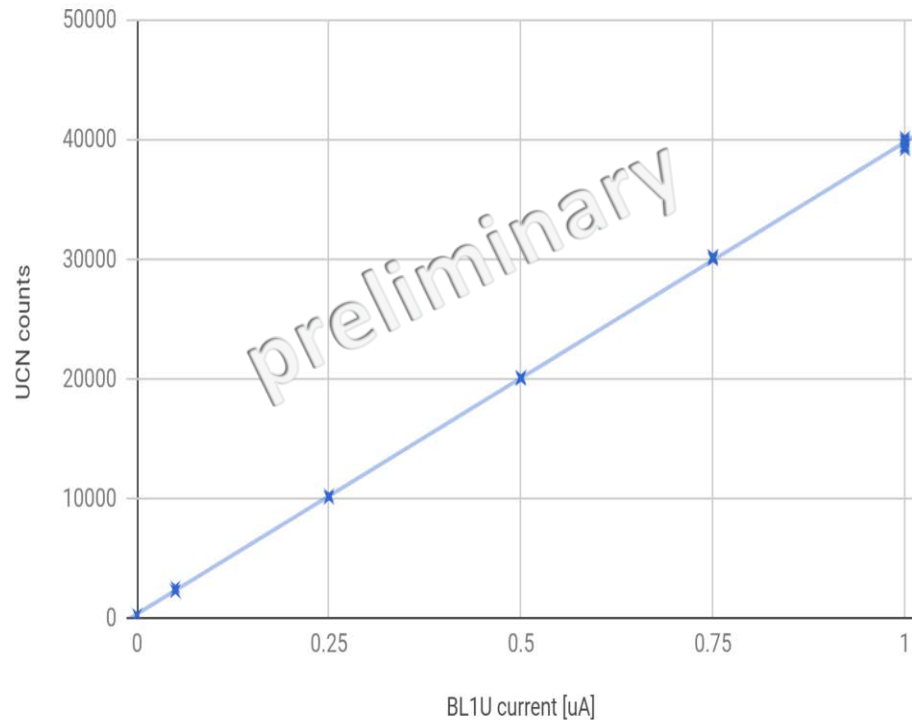
First UCN production at TRIUMF

- 2014 - 2017: installation of beamline and source
- **Nov 13, 2017: first UCN produced at TRIUMF**
- Approx. 5×10^4 per shot at $1 \mu\text{A}$ and $> 3 \times 10^5$ at $10 \mu\text{A}$
- experimental program: source and UCN hardware characterization
- UCN source is quite stable for more than one month
- **Detailed analysis is ongoing**

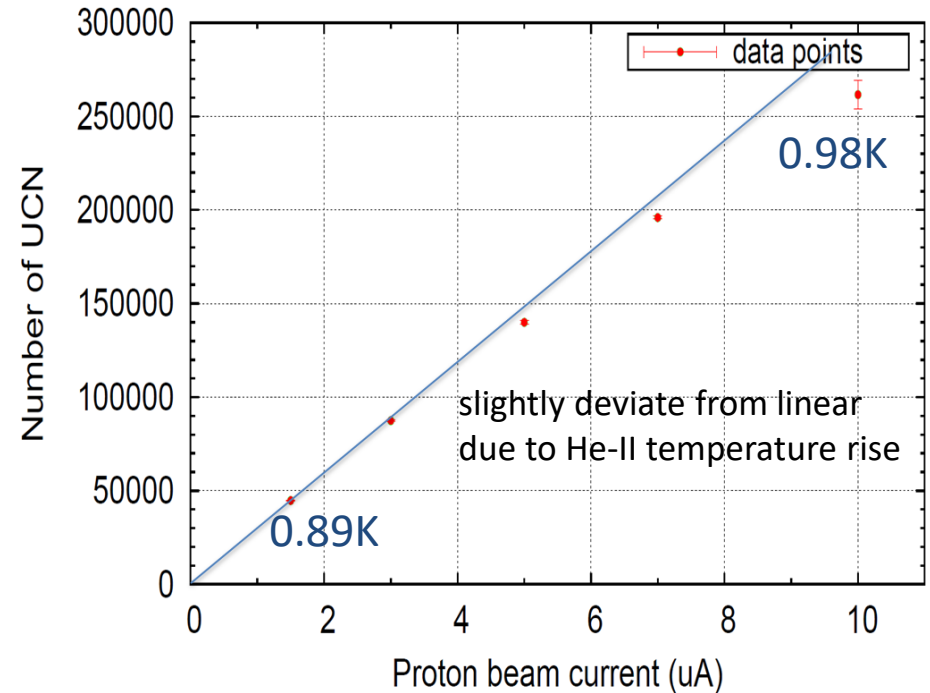


UCN will be used for R&D for Upgrading facility and EDM apparatus

UCN yield linearity in beam current



0.05 μA – 1 μA , 60 sec beam irradiation

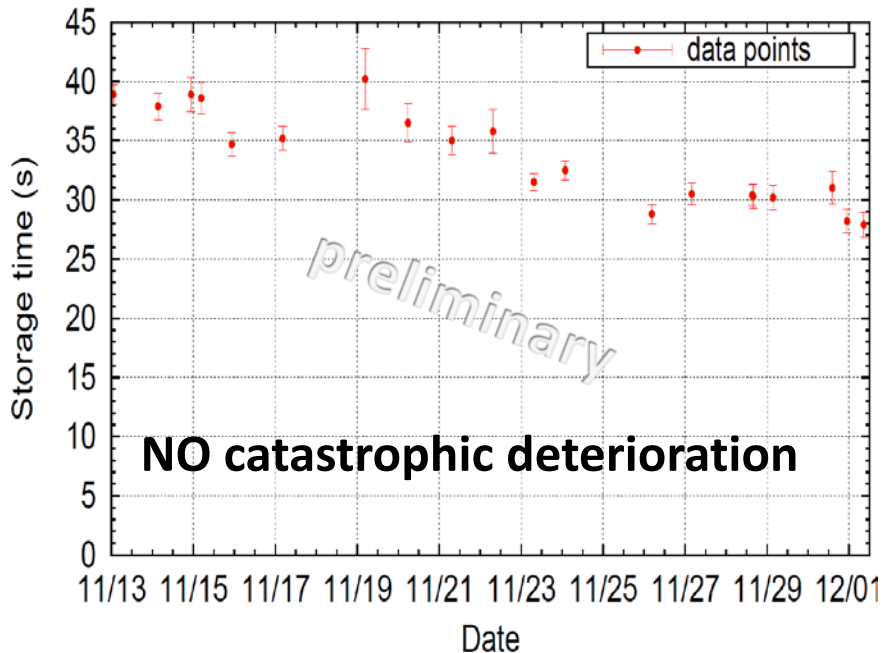


1 μA – 10 μA , 30 sec irradiation time

- Maximum UCN count rate 47000 at 1 μA (RCNP best shot 80000)
- We have non optimized UCN valve, longer UCN guides and an aluminum foil before the detector
- By far enough UCN to do our measurement program
- Vertical Source is capable of sustaining higher currents and the UCN yield can be increased significantly.
- Highest number for 60 s irradiation and 10 μA : 3.25×10^5

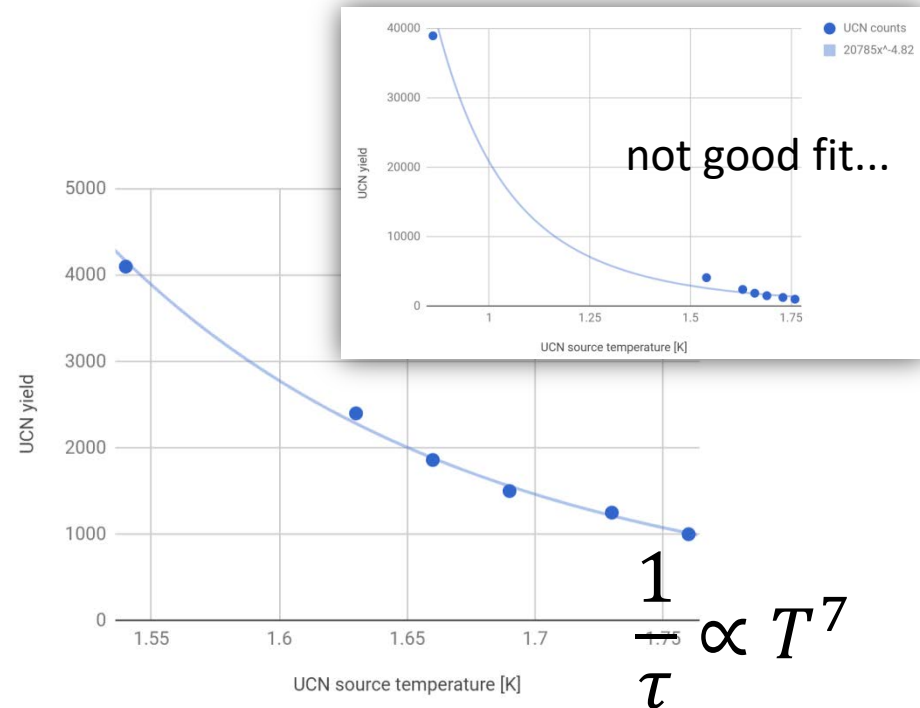
Other experimental program

Storage lifetime evolution



This is the first time we run the vertical source for more than 1 week

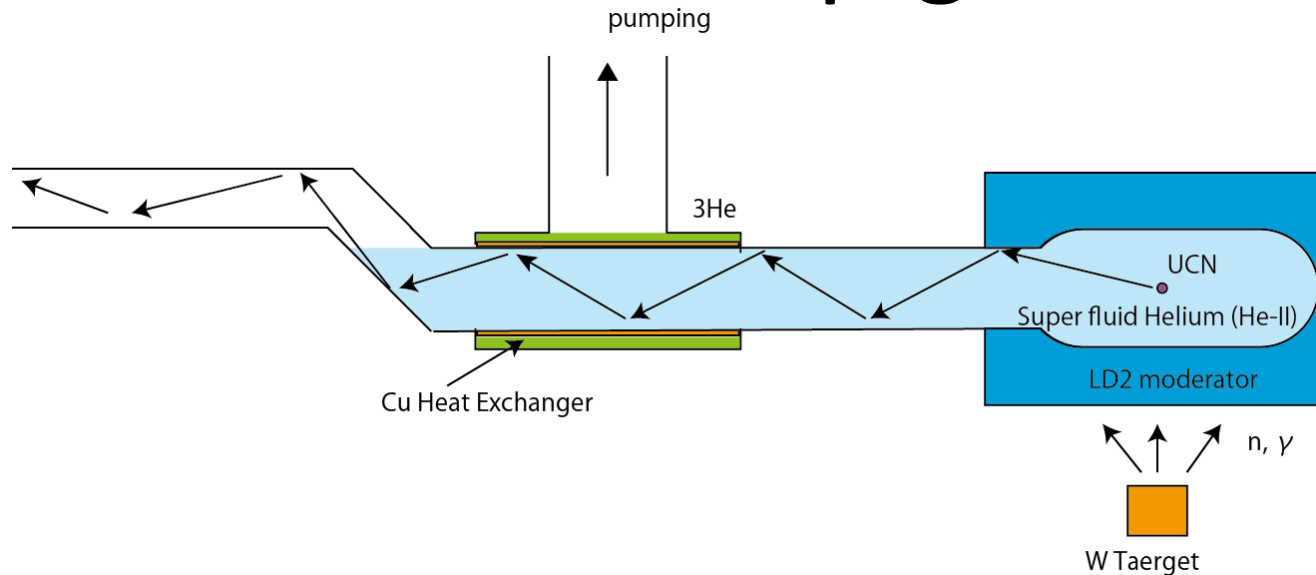
UCN production in higher temperature



- Detector characteristic (^3He gas, ^6Li grass)
- UCN guide characteristic
- and so on,

detailed analysis is ongoing

UCN source up-grade



proton beam power

0.4 kW at RCNP -> 20 kW at TRIUMF

A new helium cryostat which has high cooling power is necessary

Heat load on He-II depends on geometry

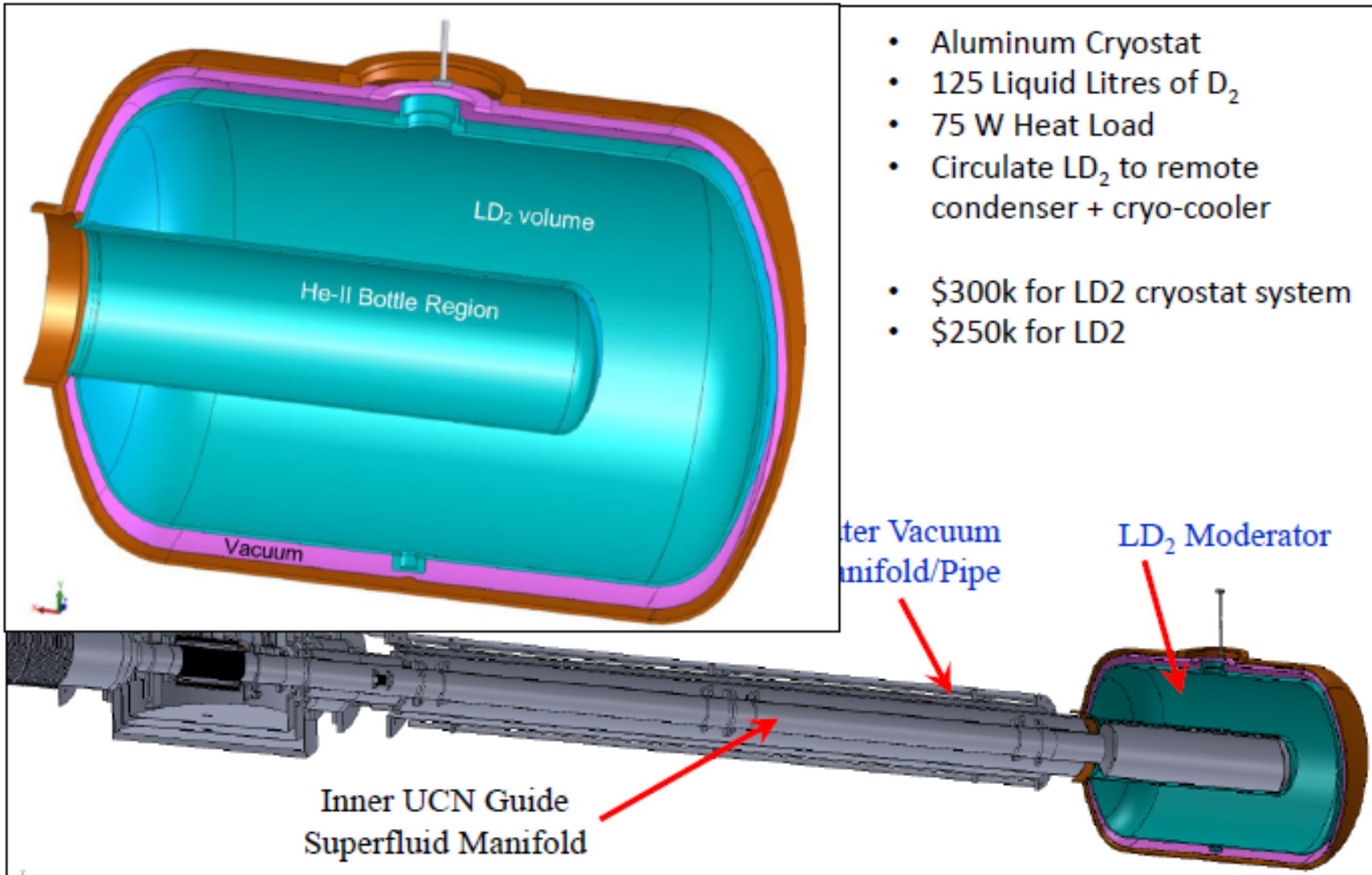
- distance between target and He-II
 - cold moderator
 - gamma shield
- and so on



- higher cold neutron flux cause higher heat load
- ratio of this is constant in some region

Optimization is necessary

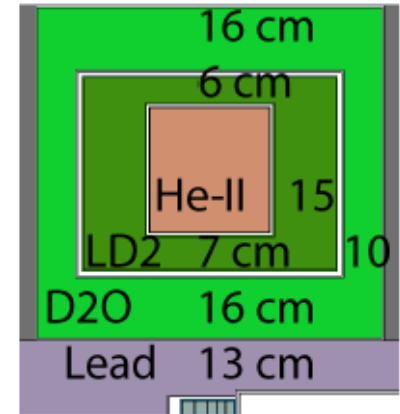
LD₂ Moderator Cryostat



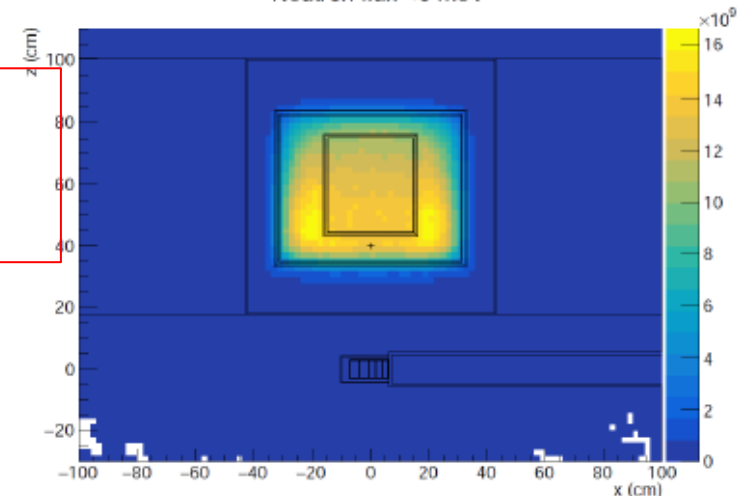
5 – 9 times larger cold neutron flux is achievable compared with ice D₂O

Heat load on UCN production volume

- Radial LD₂ layer more important than lower
- Best He-II-bottle height 30-40 cm, radius 15-20 cm (for current cooling scheme)
- Limited by amount of LD₂!
- For He-II height 30 cm, radius 15 cm, 40 μ A beam:
 - 20.6 l He-II, 115 l LD₂
 - $3.9 \cdot 10^7$ UCN/s
 - 7.9 W max. heat in He-II
 - 65 W max. heat in LD₂
- Best strategy to reduce LD₂:
reduce He-II size and go closer to target



Neutron flux <6 meV



deal with such a huge heat load around 1 K

He cryostat

- to keep He-II temp. ~ 1.0 K
- decompressed Helium 3
- ^3He vs ^4He

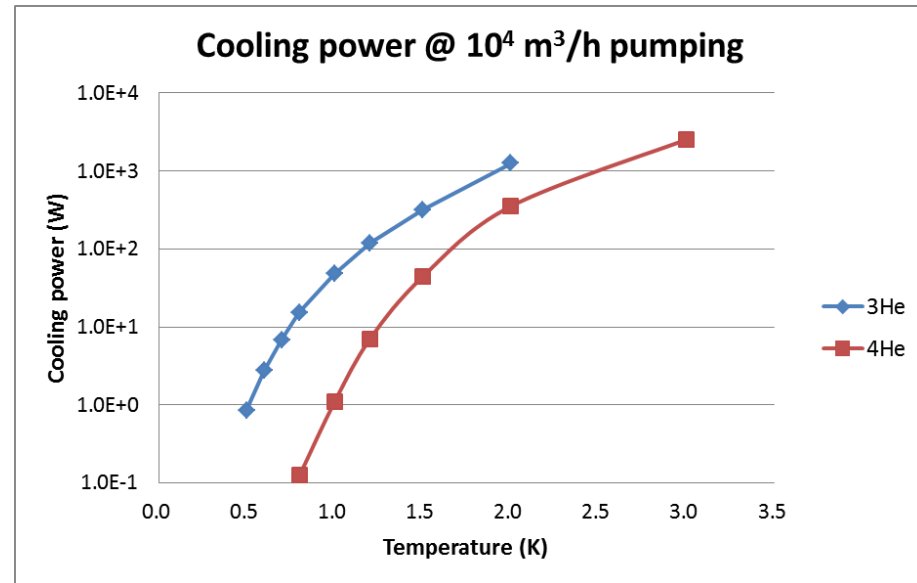
– vapor pressure @ 0.8K

- ^3He : 3 Torr
- ^4He : 0.01 Torr

– cooling power

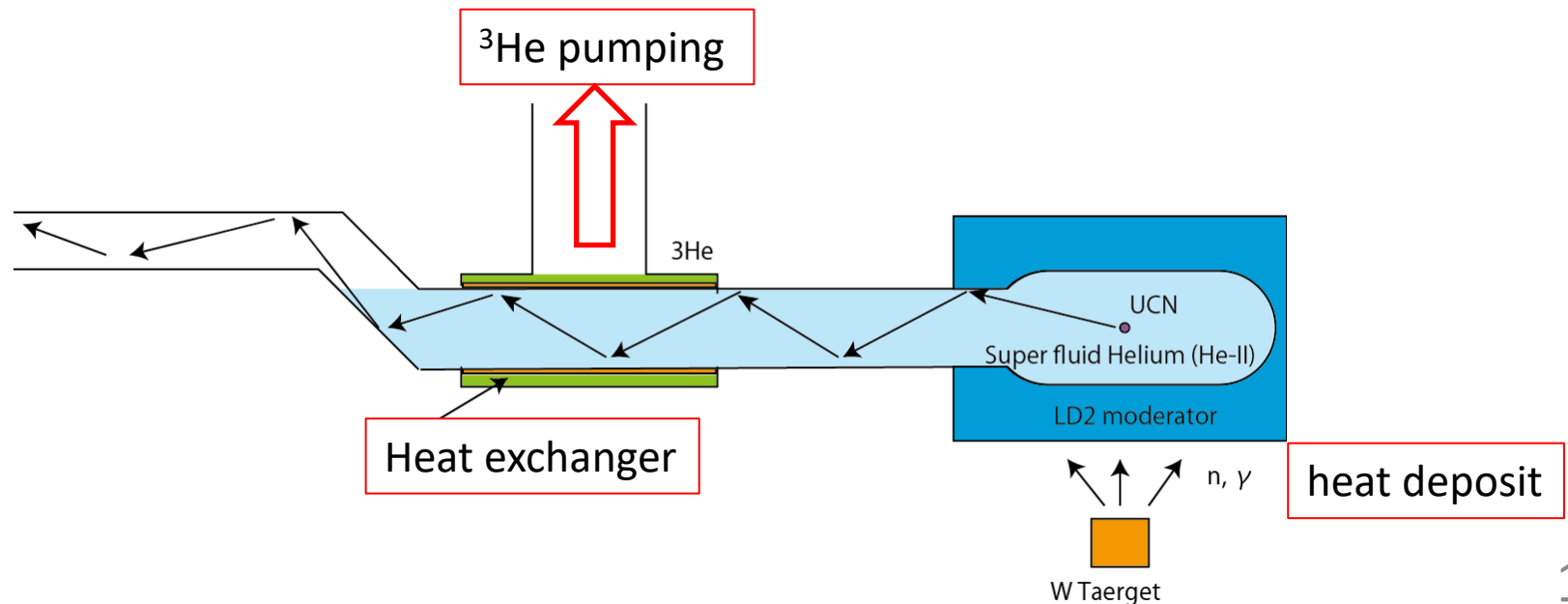
@ 0.8K with 10,000 m³/hour pumping

- ^3He : 15W
- ^4He : 0.13 W



Heat transfer between heating point and cooling point

- Heat transfer in He-II
 - below 1 K, heat transfer is not good because of low fraction of normal fluid which convey heat (two fluid model)
- Kapitza conductance of heat exchanger
 - Conductance at the surface between liquid and solid is small at low temperature

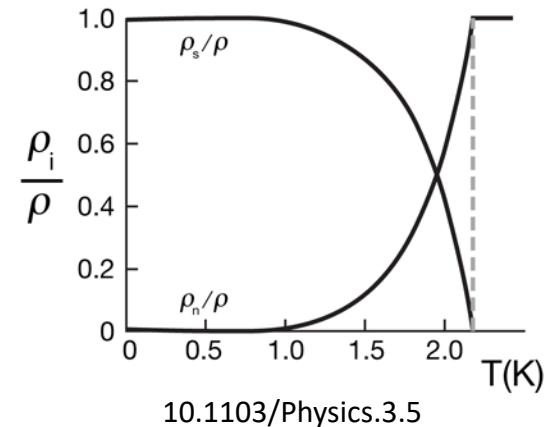


Superfluid Helium

Two Fluid Model

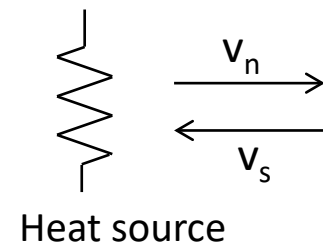
	Normal fluid	Superfluid
Viscosity	H_n	$\eta_s = 0$
Entropy	S_n	$S_s = 0$

- Ratio of super/normal component depends on temperature.
- fraction of normal mode become small in low temperature.



Heat transport

- Since superfluid has no entropy, heat is transported only by normal fluid.
- Heat transport in low temperature ($< 1\text{K}$) become small because of small fraction of normal fluid



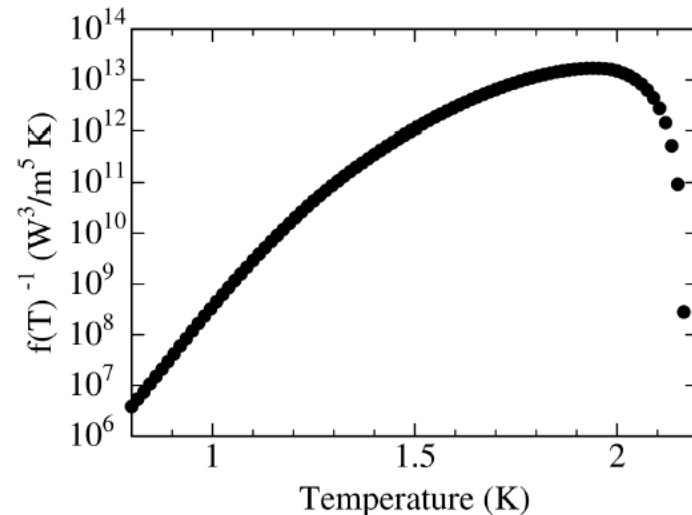
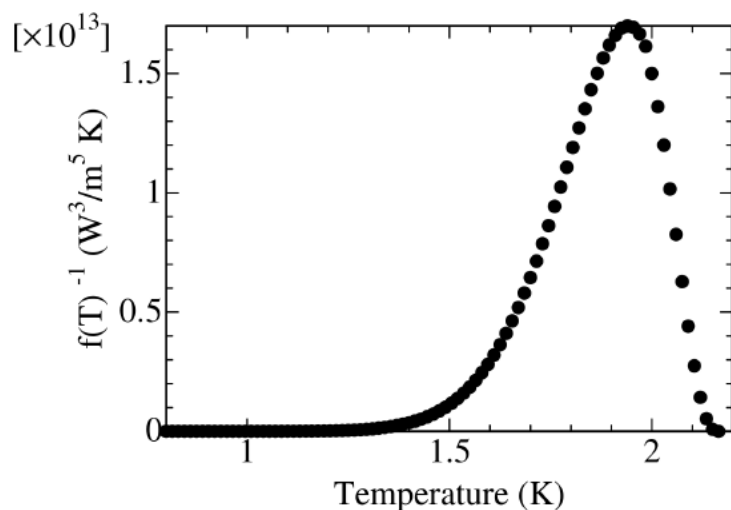
Gorter-Mellink Equation

$$q_j(\mathbf{r}) = - \left(f(T)^{-1} \frac{\partial T(\mathbf{r})}{\partial x_j} \right)^{1/3}, \quad f(T) = \frac{A_{gm} \rho n}{\rho_s^3 s^4 T^3}$$

$q_j(\mathbf{r})$: [W/m^2] Heat Flux vector at \mathbf{r} .

$f^{-1}(T)$: [$\text{W}^3/\text{m}^5 \text{K}$] Heat transfer function. ($\Leftrightarrow q_j = -\lambda \partial_j T$)

A_{gm} : Gorter-Mellink mutual friction parameter, [$\text{m}\cdot\text{sec}$].



$f(T)^{-1}$: Heat transfer function of He-II based on Two fluid model

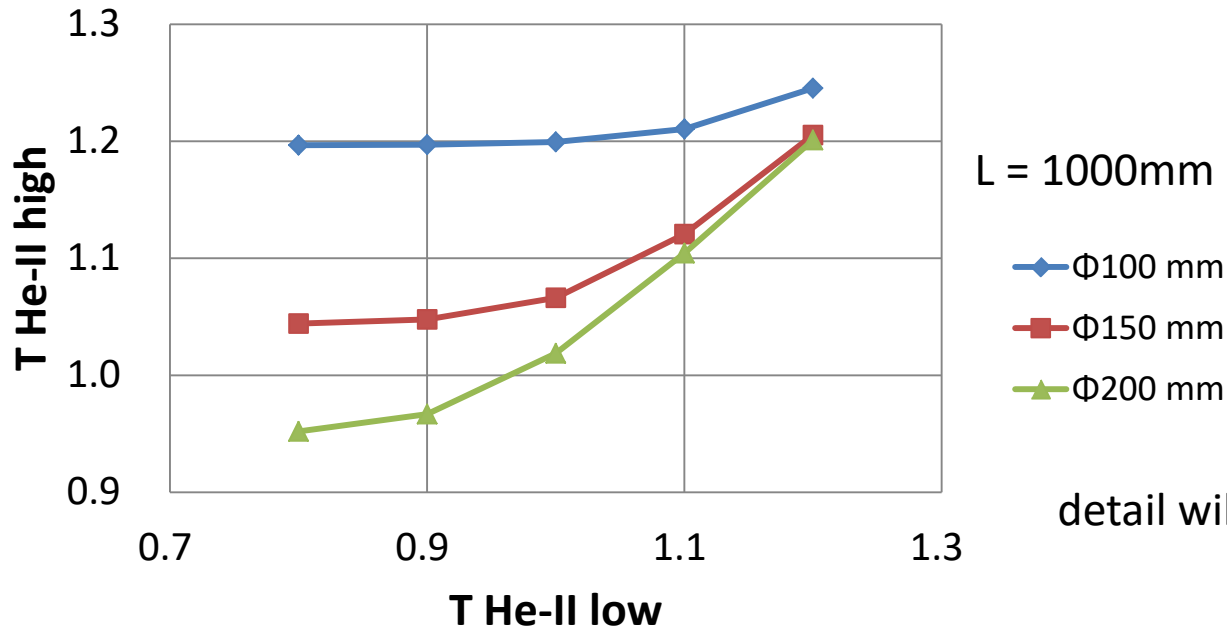
Temperature difference in He-II

Chamber temperature, T_H , can be solved numerically using following Gorter-Mellink equation.

$$Q_{in} = \left(\frac{A^3}{L} \int_{T_L}^{T_H} f(T)^{-1} dT \right)^{1/3}$$

A : cross section of He-II
L : distance of heat transfer

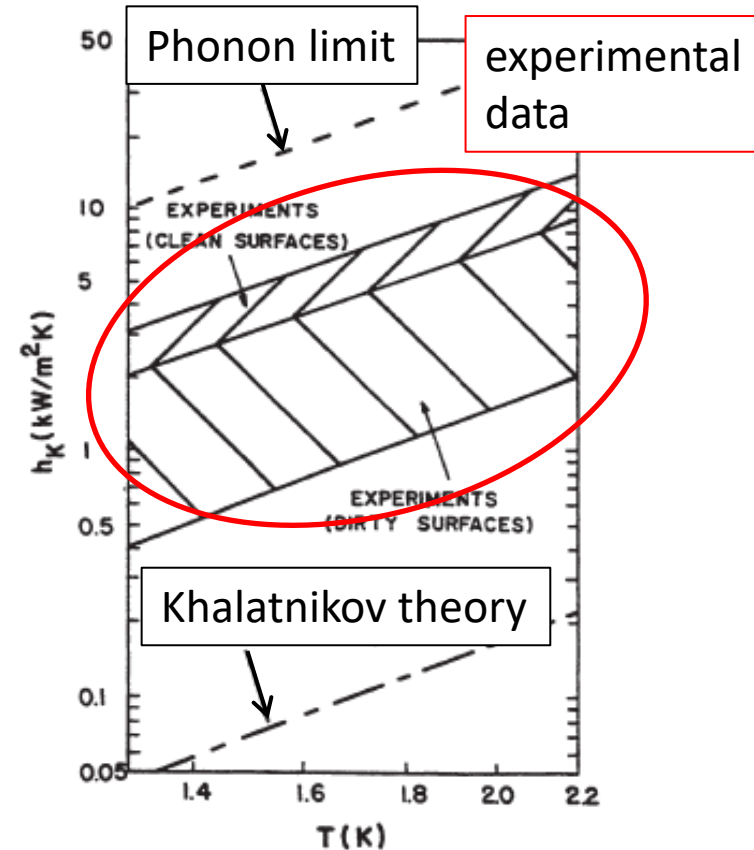
Temperature increase in He-II
10 W heat load



detail will be discussed by T. Okamura

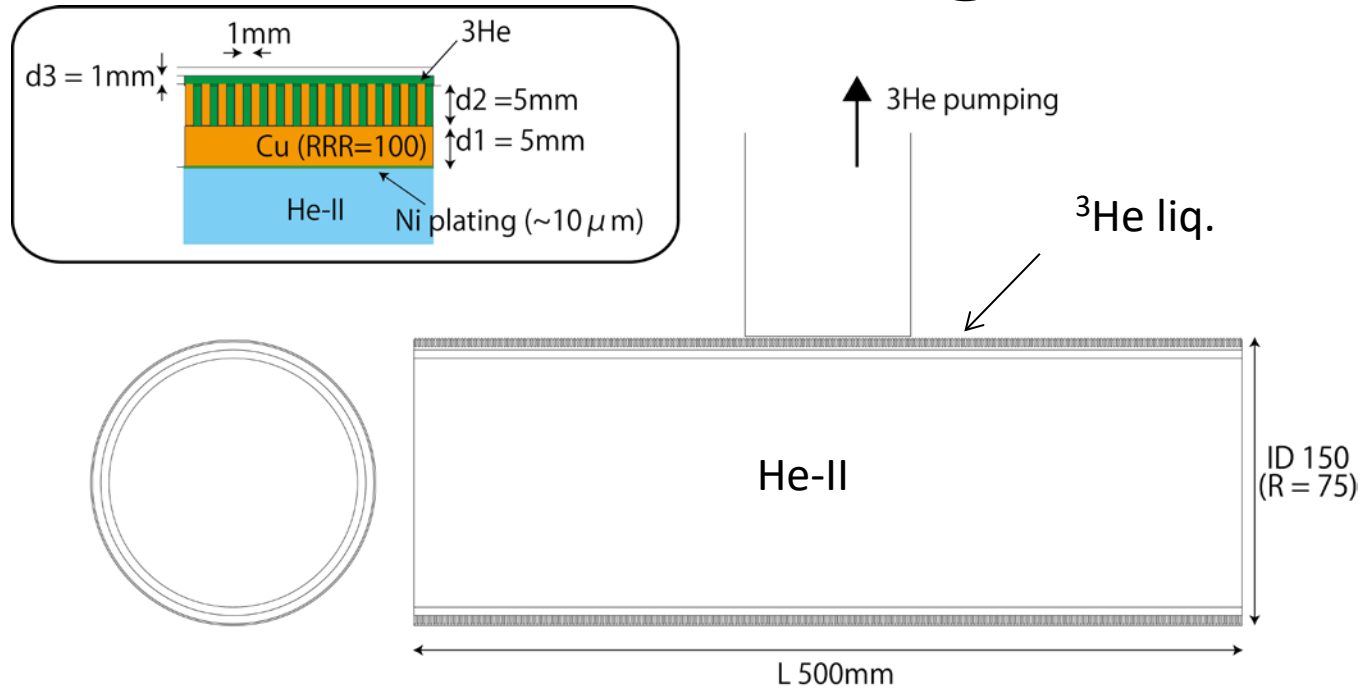
Kapitza Conductance

- Kapitza conductance is Conductance at the junction between liquid and solid is small at low temperature
- Kapitza conductance, $h_K(T)$ is a function of temperature.
- There are several theory on Kapitza conductance.
 - Phonon limit
 - $h_K(T) \sim 4500 T^3$ [W/m²K]
 - 2 - 10 times larger than measured
 - Khalatnikov theory
 - $h_K(T) \sim 20 T^3$ [W/m²K]
 - 10 - 100 times smaller than measured
- Experimental data strongly depends on surface quality
 - plan to measure Kapitza conductance at KEK



Kapitza conductance
between Copper and He-II
Helium cryogenics, Steven W. Van Sciver

Heat exchanger



Cu Heat exchanger should be plated by Ni
Kapitza conductance between Cu-Ni is large enough since junction is solid-solid

- Kapitza conductance between Ni and He-II

$$h_{K Ni}(T) = f \cdot h_{K Cu}(T) \quad f = 0.61$$
- Kapitza conductance between Cu and 3He

$$h_K(\text{HeII}) = (1.2 - 2.6) h_K(3\text{He})$$

ex) average quality of Cu, 10 W heat load

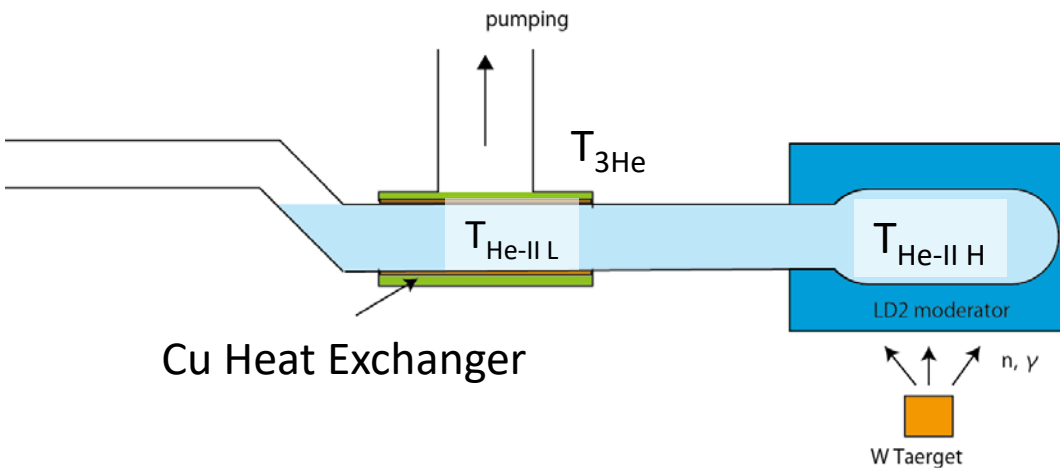
- junction between He-II and Ni
 - $h_{K Ni}(1.0\text{K}) = 244 \text{ [w/m}^2 \text{ K]}$
 - $\Delta T_{\text{He-II} - \text{Ni}} = 0.16 \text{ K}$
 - $T_{\text{Ni}} = 0.84 \text{ K}$
- junction between Cu and 3He
 - $h_{K Ni}(0.84\text{K}) = 232 \text{ [w/m}^2 \text{ K]}$
 - $\Delta T_{\text{He-II} - \text{Ni}} = 0.09 \text{ K}$
 - $T_{3\text{He}} = 0.75 \text{ K}$

Equilibrium temperature

Equilibrium temperature can be calculated as a function heat load.

example)

$d = 150 \text{ mm}$, $L = 1,500 \text{ mm}$
pumping speed $10,000 \text{ m}^3/\text{hour}$
Heat load : 10 W case



Temperature distribution

$T_{\text{He-II H}} : 1.15 \text{ K}$ ($\tau_{\text{up-scat}} = 50 \text{ sec}$)

$T_{\text{He-II L}} : 1.00 \text{ K}$

$T_{\text{Cu H}} : 0.84 \text{ K}$

$T_{\text{Cu L}} : 0.83 \text{ K}$

$T_{3\text{He}} : 0.75 \text{ K}$

$\Delta T = 0.40 \text{ K}$

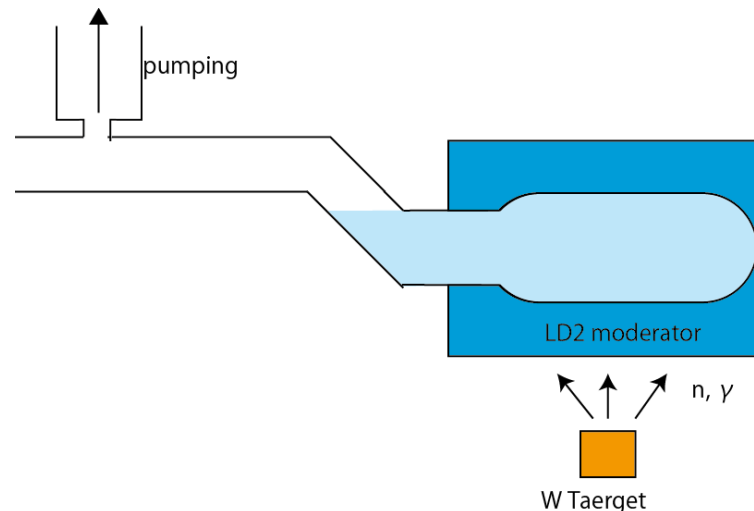
Large uncertainty in parameter (Kapitza, GM)

-> have to be tested

-> we will have experiments at the beginning 2018

Alternative plan : direct pumping

- direct pumping of He-II
 - another way to cooldown He-II
 - There is no effect of Kapitza conductance since they have no heat exchanger
 - if Kapitza conductance is found to be smaller than expected, the direct pumping have large advantage
 - He-II volume can be small
 - temperature difference in He-II become small
 - Cooling power : 7 W at 1.2 K with 10,000 m³/hour pumping
 - upscattering life time at 1.2 K : 36 sec



High cooling power cryostat

- A new He-II cryostat is being developed
 - TRIUMF proton beam line BL1U
 - $500 \text{ MeV} \times 40 \mu\text{A} = 20 \text{ kW}$
 - necessary cooling power is around 10 W at 1.0 K
 - Heat conductance is important
 - inside He-II
 - Kapitza conductance between He-II/³He and heat exchanger
- Isopure ⁴He direct pumping is an alternative method

Expected statistics after UCN source upgrade

- New He cryostat will be made for 20 kW operation
- LD2 moderator increase cold neutron flux by factor 5 – 9
- UCN guide coating facility will be established at U. Winnipeg

	vertical source	horizontal source	factor
proton beam	0.4 kW	20 kW	× 50
production volume	8 L	12 L	× 1.5
LD2 moderator	-	-	× 5 – 9
UCN production rate	3.2×10^4 UCNs	2.3×10^7 UCN/s	~ 700

statistical sensitivity

$$\sigma_d = \frac{\hbar}{2\alpha E t_c \sqrt{N}}$$

E = 10kV/cm

$t_c = 130$ s

$\alpha = 0.8$ (visibility)

N : number of UCN

$\rho = 680$ Pol. UCN/cm³ @20kW operation, TRIUMF

in cell of ϕ 36 cm and H 15 cm (15L) × double cell

N = 2.1×10^7 UCN/batch

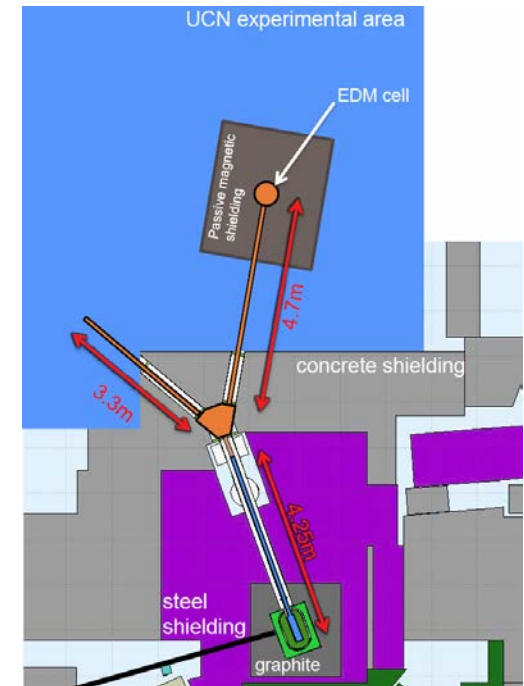
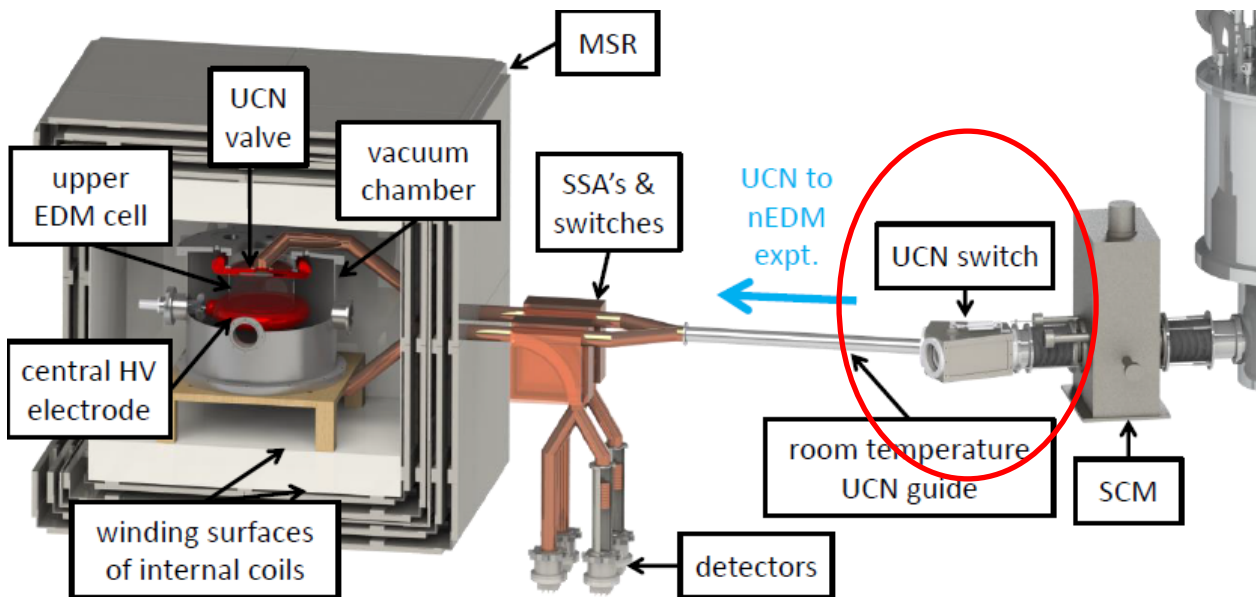
$$\sigma_d = 5.6 \times 10^{-26} \text{ ecm/cycle}$$

(1 cycle : 8 fill to determine the resonant frequency)

assume stable running of 14 hours/day

$$\sigma_d = 1 \times 10^{-27} \text{ ecm/100 MT day}$$

Second UCN port : Y switch



beamline layout

- Bend is necessary for radiation protection
 - to not see target area directly
- Y switch can divert UCN to second area.
 - R&D for UCN guide, detector and so on
 - open for user facility in future

If you have an interest idea to use UCN, please contact us!!

Summary

- High UCN density is essential to overcome current limit of neutron EDM measurement sensitivity
- UCN production in superfluid helium is a viable way to achieve a high density UCN source
- UCN production with the vertical UCN source succeeded
 - will use UCN produced for R&D for source and nEDM experiment
- High intensity UCN source is being developed
 - proton beam power : $500 \text{ MeV} * 40 \text{ } \mu\text{A} = 20 \text{ kW}$
 - new cryostat with higher cooling power
 - necessary cooling power : $\sim 10 \text{ W}$ at 1.0 K
 - ^3He pumping, isopure ^4He pumping
 - Final optimization is ongoing
 - statistical error of $10^{-27} \text{ ecm} / 100 \text{ MT day}$
 - Plan to produce UCN from 2021

